HAYNES® HR-235® Alloy

Principal Features

HAYNES[®] HR-235[®] alloy is a nickel-chromium-molybdenum-copper material with outstanding resistance to metal dusting. It has no deliberate addition of iron, an element which is detrimental to the performance of alloys under metal dusting conditions. It is resistant to creep-rupture at temperatures under which metal dusting is normally encountered. Having a low silicon and aluminum content, HR-235[®] alloy is resistant to weld solidification and strain-age cracking. This is an improvement over other alloys intended for metal dusting resistance. It is also available as a filler wire with matching composition.

Applications:

- Petrochemical Plants
- Syngas production
- Synthesis of ammonia, methanol, LNG, H₂
- Microchannel High Temperature Reactors
- High carbon containing gases
- Direct reduction of iron ores
- Carbon fiber production
- Gas-to-liquids (GTL) plants
- Steam-methane-reforming process

Nominal Composition

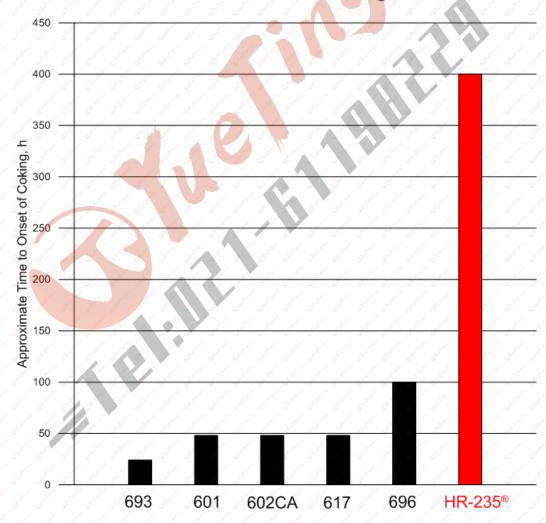
	int %
Nickel:	Balance
Chromium:	31
Molybdenum:	5.6
Copper:	3.8
Iron:	1.5 max
Niobium:	1.0 max
Aluminum:	0.4 max
Manganese:	0.65 max
Silicon:	0.6 max
Titanium:	0.5 max
Carbon:	0.06 max

Weight %

Meltal Dusting

HAYNES[®] HR-235[®] alloy has been tested alongside competitive materials in a controlled atmosphere, thermal cycling rig. The reaction gas was $H_2 + 68\%$ CO + 6% H_2 O, the carbon activity of which was 2.9 at the reaction temperature. The cycling operation, which was controlled automatically, comprised 45 minutes at the reaction temperature of 1256°F (680°C), followed by a cooling period of 15 minutes, during which the samples rapidly reached a temperature of about 194°F (90°C). The samples were tested for 1,200 (one hour) cycles, with the following results. The formation of filamentary carbon deposits with metallic nanoparticles (coking) is an indicator of the onset of surface damage (pitting).

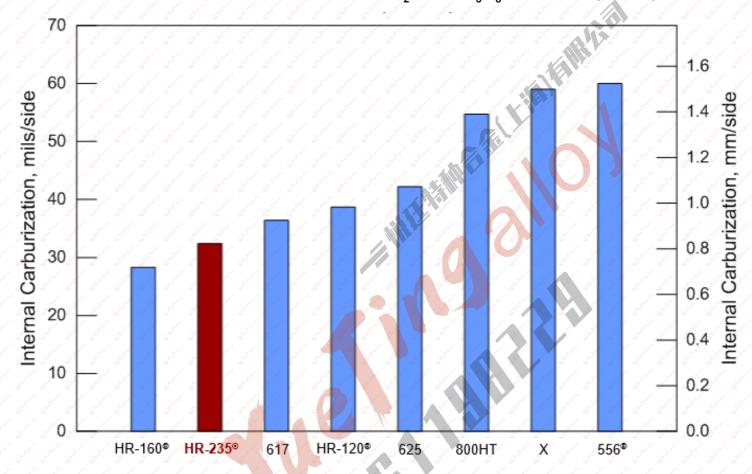
Alloy	Approximate Number of Cycles to Coking	Form of Coke
601	48	Grain boundary deposits, pits
602CA	48	Adherent coke, no metal visible
617	48	Numerous small pits, grain boundary deposits
693	24	Numerous small pits
696	100	Attack on grain boundaries
HR-235 [®]	400	Grain boundary deposits, minor pits



Time to Onset of Coking, h

Carburization Resistance

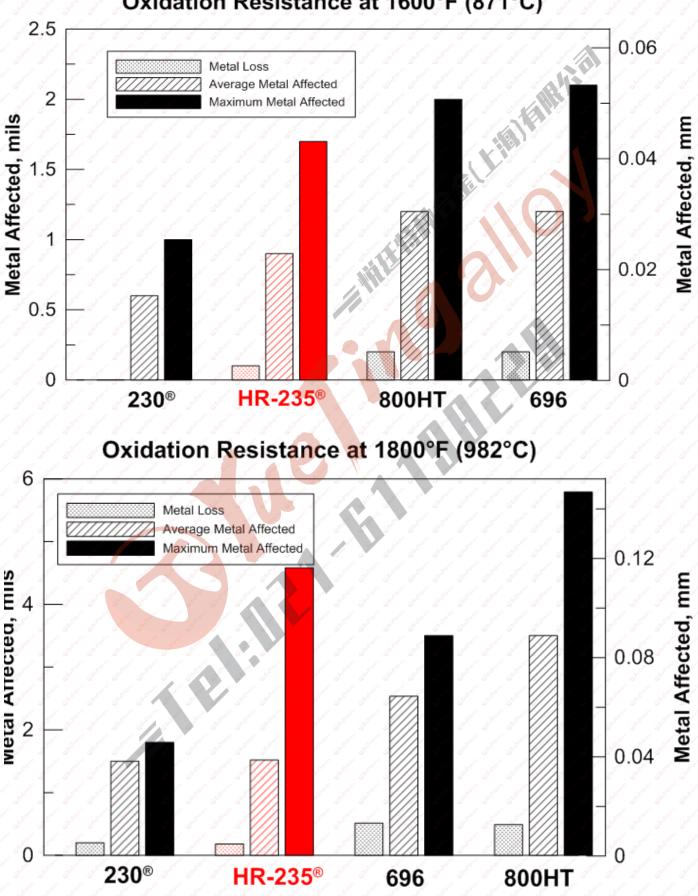
In addition to its high resistance to metal dusting, HAYNES[®] HR-235[®] alloy also withstands carburization, a degradation process which occurs at lower carbon activities and which negatively affects many metallic materials, as shown in the following chart. The test involved a gas mixture of Ar – 5% H₂ – 2% C₃H₈ at 1800°F (982°C), with a carbon activity of 1; the test duration was 215 h.



Internal Carburization in Ar– 5% $H_2 - 2\% C_3 H_8$ at 1800°F (982°C)

Oxidation Resistance

HAYNES® HR-235® alloy also exhibits good oxidation resistance, as indicated in the following chart. The test was performed in flowing air (55.5 cm³/s) for 1,008 h, with an air cool to room temperature every 168 h.



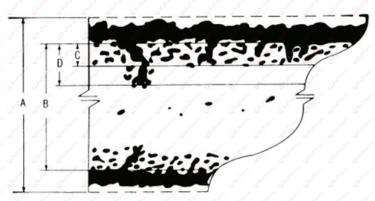
Oxidation Resistance at 1600°F (871°C)

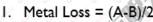
Haynes International - HAYNES® HR-235® alloy

Oxidation Resistance Continued

Measurement of High Temperature Corrosion Attack

To assess the extent of attack (internal and external) of materials caused by oxidation, the following measurements are taken, using metallographic techniques, where A is the original thickness of the sample.

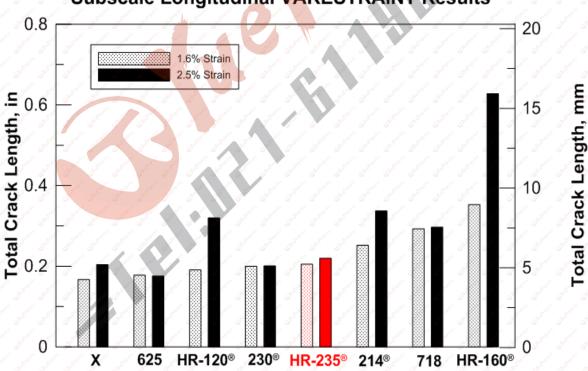




- 2. Average Internal Penetration = C
- 3. Maximum Internal Penetration = D
- 4. Average Metal Affected = [(A-B)/2] + C
- 5. Maximum Metal Affected = [(A-B)/2] + D

Weld Solidification Cracking Resistance

HAYNES[®] HR-235[®] alloy is resistant to weld solidification cracking, as measured by the VARESTRAINT weldability test. Materials with significant silicon contents, such as HR-160[®] alloy, are prone to this form of cracking, as a result of their wider melting ranges. Having a low silicon and aluminum content, HR-235[®] alloy is resistant to weld solidification and strain-age cracking. This is an improvement over other alloys intended for metal dusting resistance. It is also available as a filler wire with matching composition. For more information, visit our Welding and Fabrication Brochure.



Subscale Longitudinal VARESTRAINT Results

Physical Property	Briti	sh Units	Metri	c Units
Density	RT	0.295 lb/in ³	RT	8.16 g/cm ³
Melting Range	ting Range 2401-2437°F		1316-1356°C	Start Start Start Start Start
enarch enarch enarch enarch enarch	RT	48.4 µohm-in	RT	1.23 µohm-m
den Stan Stan Stan Stan Stan Stan	200°F	48.8 µohm-in	100°C	1.24 µohm-m
and and and an an an	400°F	49.2 µohm-in	200°C	1.25 µohm-m
perior start start start start	600°F	49.6 µohm-in	300°C	1.26 µohm-m
inform Staffor Stafford Stafford Stafford Stafford	800°F	50.4 µohm-in	400°C	1.27 µohm-m
Electrical	1000°F	50.8 µohm-in	500°C	1.29 µohm-m
Resistivity -	1200°F	50.4 µohm-in	600°C	1.29 µohm-m
aller and and all all all all all all all all all al	1400°F	50.4 µohm-in	700°C	1.28 µohm-m
and along some and a source as	1600°F	50.4 µohm-in	800°C	1.28 µohm-m
Stand Stand Stand Stand Stand	1800°F	50.4 µohm-in	900°C	1.28 µohm-m
en Str. Str. Str. Str. Str enter enter and enter and	2000°F	51.2 µohm-in	1000°C	1.28 µohm-m
nt and all and all all all	RT	70 BTU.in/h.ft ² .°F	RT	10.0 W/m.°C
at other other other other other	200°F	77 BTU.in/h.ft ² .°F	100°C	11.0 W/m.°C
and Starting Starting Starting Starting	400°F	89 BTU.in/h.ft ² .°F	200°C	12.5 W/m.°C
alan Stater States States States	600°F	101 BTU.in/h.ft ² .°F	300°C	14.2 W/m.°C
And Share Share Share Share Share	800°F	114 BTU.in/h.ft ² .°F	400°C	15.8 W/m.°C
Thermal	1000°F	125 BTU.in/h.ft ² .°F	500°C	17.3 W/m.°C
Conductivity -	1200°F	137 BTU.in/h.ft ² .°F	600°C	18.9 W/m.°C
And Martin States And Martin States	1400°F	150 BTU.in/h.ft ² .°F	700°C	20.6 W/m.°C
Alterna and the second and the second and the	1600°F	153 BTU.in/h.ft ² .°F	800°C	21.6 W/m.°C
and an	1800°F	164 BTU.in/h.ft ² .°F	900°C	22.3 W/m.°C
en der der der der der ander ander	2000°F	174BTU.in/h.ft ² .°F	1000°C	23.5 W/m.°C
n an	70-200°F	6.8 µin/in.°F	25-100°C	12.3 µm/m.°C
and the start start start start	70-400°F	7.1 µin/in.°F	25-200°C	12.8 µm/m.°C
an share share share share stare	70-600°F	7.4 µin/in.°F	25-300°C	13.2 µm/m.°C
after States States States States	70-800°F	7.5 µin/in.°F	25-400°C	13.5 µm/m.°C
Mean Coefficient	70-1000°F	7.7 µin/in.°F	25-500°C	13.8 µm/m.°C
of Thermal	70-1200°F	8.1 µin/in.°F	25-600°C	14.2 µm/m.°C
Expansion -	70-1400°F	8.4 µin/in.°F	25-700°C	14.7 µm/m.°C
And share after a start and	70-1600°F	8.7 µin/in.°F	25-800°C	15.2 µm/m.°C
Start Martin Martin Start Start	70-1800°F	9.0 µin/in.°F	25-900°C	15.7 µm/m.°C
t 3° 3° 3° 3° 3° 3° 3° 4° 4° 4° 4°	70-2000°F	9.3 µin/in.°F	25-1000°C	16.2 µm/m.°C

Physical Properties

Physical Property	Britis	h Units	Metric	Units
and a start of the	RT	0.108 ft²/h	RT	0.0279 cm ² /s
all and a second and a second and a	200°F	0.116 ft²/h	100°C	0.0299 cm²/s
and an an an an an an	400°F	0.127 ft²/h	200°C	0.0328 cm ² /s
and and and and and and	600°F	0.139 ft²/h	300°C	0.0356 cm ² /s
the strength of the strength os strength of the strength os streng	800°F	0.151 ft²/h	400°C	0.0382 cm ² /s
Thermal – Diffusivity –	1000°F	0.162 ft²/h	500°C	0.0408 cm ² /s
Dillusivity	1200°F	0.173 ft²/h	600°C	0.0434 cm²/s
States States States States States States States	1400°F	0.183 ft²/h	√ 700°C	0.0459 cm ² /s
Stand Stand Stand Stand Stand Stand	1600°F	0.182 ft²/h	800°C	0.0470 cm ² /s
and and a second and a second and a second at	1800°F	0.191 ft²/h	900°C	0.0475 cm²/s
stand stand stand stand stand stand	2000°F	0.200 ft²/h	1000°C	0.0495 cm ² /s
and	RT	0.105 BTU/lb.°F	RT	440 J/kg.°C
all and all all all all all all all all all al	200°F	0.109 BTU/lb.°F	100°C	456 J/kg.°C
2° 3° 3° 3° 3° 3° 3° 3° 3° 3° 3° 3° 3° 3°	400°F	0.114 BTU/lb.°F	200°C	477 J/kg.°C
	600°F	0.119 BTU/lb.°F	300°C	494 J/kg.°C
Start Start Start Start Start Start Start	800°F	0.124 BTU/lb.°F	400°C	511 J/kg.°C
Specific Heat	1000°F	0.133 BTU/lb.°F	500°C	532 J/kg.°C
State State State State State State State	1200°F	0.148 BTU/lb.°F	600°C	611 J/kg.°C
Statement Statement Statement Statement Statement	1400°F	0.146 BTU/lb.°F	700°C	620 J/kg.°C
Salar Salar Salar Salar Salar Salar Salar Salar	1600°F	0.152 BTU/lb.°F	800°C	615 J/kg.°C
Stand Stand Stand Stand Stand	1800°F	0.152 BTU/lb.°F	900°C	641 J/kg.°C
and	2000°F	0.153 BTU/lb.°F	1000°C	624 J/kg.°C
and the and the and the and the and the and	RT	29.0 x 10 ⁶ psi	RT	200 GPa
Start Start Start Start Start	200°F	28.5 x 10 ⁶ psi	100°C	196 GPa
and and an an and and and and	400°F	27.6 x 10 ⁶ psi	200°C	191 GPa
den den den den den den den den	600°F	26.7 x 10 ⁶ psi	300°C	184 GPa
Dynamic Modulus 🗌	800°F	25.9 x 10ºpsi	400°C	180 GPa
of Elasticity	1000°F	25.0 x 10⁵psi	500°C	174 GPa
Sala Sala Sala Sala Sala Sala Sala Sala	1200°F	23.9 x 10 ⁶ psi	600°C	168 GPa
and and and and an and and	1400°F	23.0 x 10 ⁶ psi	700°C	162 GPa
select select select select select a	1600°F	21.3 x 10⁵psi	800°C	154 GPa
statement statement statement statement statement		Start statement statement - statement statement	900°C	144 GPa

Physical Properties Continued

Tensile Properties

Tempe	rature	Yield Strength 0.2% Offset		Ultimate Strei	Elonga tion	
°F	°C	ksi	MPa	ksi	MPa	%
RT	RT	48.8	337	106.9	737	58
1000	538	29.5	203	81.6	562	63
1200	649	28.7	198	72.7	61	
1400	760	27.7	191	56.5	389	67
1600	871	22.4	154	31.3	216	72
1800	982	11.3	78	16.4	113	72

HAYNES® HR-235® Solution Annealed Plate

Creep and Stress Rupture Strength

HR-235[®] Solution Annealed Plate*

Tempe	erature	Creep	Approxima		ess to Produc ep in:	e Specified
°F	°C		100) h	10	00 h 📝 🗸
Server Martin		%	ksi	MPa	ksi	MPa
1000	E20		57	393	45	310
1000	538	Rupture	81 🦲	558	58	400
1100	502	1//	40	276	30	207
1100	593	Rupture	56	386	38	262
1000	640	1/1//	27	186	19	131
1200	649	Rupture	38	262	24	165
1200	704	1	17	117	11	76
1300	704	Rupture	25	172	15	103
1400	760	1 × 1 × ×	10	69	6	41
1400	760	Rupture	16	110	9	62
1500	016	1	6	41	4	28
1500	816	Rupture	ه 🏷 10 🗸 ه	69	6 6	41
1000	071	3 ⁵⁰ 3 ⁵¹ 1 3 ⁵¹ 3 ⁵¹	4 / 4	28	8 8 2 8 v	14
1600	871	Rupture	6 / 3	41 /	6 6 4 6	28
1700	007	1	2 0 0	14 🧹 🖌	a sure sure lare sure .	/ / / /
1700	927	Rupture	4	28	2	14

*Preliminary data

Hardness and Grain Size

HAYNES® HR-235® Alloy

Form	Solution Annealed Room Temperature Hardness	Typical ASTM Grain Size
Sheet	87 HRB	2-4
Plate	85 HRB	2-4

Heat Treatment

Wrought HAYNES[®] HR-235[®] alloy is furnished in the solution heat treated condition, unless otherwise specified. The alloy is normally solution heat-treated at 2100-2150°F (1149-1177°C) at a time to commensurate with thickness and rapidly cooled or water quenched for optimal properties.

Welding

HAYNES[®] HR-235[®] alloy is readily weldable by Gas Tungsten Arc (GTAW) and Gas Metal Arc (GMAW) welding processes. For sheet welds and plate root passes, GTAW is suggested. For plate welds, GMAW is preferred. For GMAW, the pulsed spray transfer mode (GMAW-P) is highly suggested. The GMAW-P transfer mode is a stable, low spatter spray transfer at average current levels significantly below that for conventional spray transfer. This results in low-to-moderate weld heat input, which is important to maintain the material properties of Ni-base alloys. Submerged arc welding (SAW) is not recommended as this process is characterized by high heat input to the base metal and slow cooling of the weld. The welding characteristics of HR-235[®] alloy are comparable to the highly weldable "C-type" alloys and the same general welding guidelines apply. Compared to other metal dusting resistant Ni-base alloys, HR-235[®] alloy exhibits excellent weldability. For further welding details, please refer to the the Welding and Fabrication guide, which contains general welding guidelines applicable to HR-235[®] alloy.

Heat Treatment

Wrought forms of HR-235[®] alloy are furnished in the solution annealed condition, unless otherwise specified, and should be welded in this condition. Welding of cold-worked materials is strongly discouraged, since it accelerates precipitation of secondary phases and induces residual stresses. As such, a full solution anneal in the range of 2100-2150°F (1149-1177°C), depending on specific requirements, followed by rapid air cool or water quench is suggested. Water quenching is recommended when annealing heavy section components and cold-worked structures prior to welding.

Base Metal Preparation

The joint surface and adjacent area should be thoroughly cleaned before welding. All grease, oil, crayon marks, sulfur compounds, and other foreign matter should be removed. Contact with copper or copper-bearing materials in the joint area should be avoided. It is preferable, but not necessary, that the alloy be in the solution-annealed condition when welded.

Filler Metal Selection

For GTAW and GMAW, HR-235[®] bare filler wire is suggested. For dissimilar metal welds involving HR-235[®] alloy, please consult with Haynes International for suggested filler metals.

Welding Continued

Preheating, Interpass Temperatures, and Postweld Heat Treatment

Preheat is not required and is generally specified as room temperature. Preheat should not be used if the base metal to be welded is above 32°F (0°C). To minimize the precipitation of second phases in regions affected by the heat of welding, a maximum interpass temperature of 200°F (93°C) is recommended for HR-235[®] alloy. Auxiliary cooling methods may be used between weld passes, as needed, providing that such methods do not introduce contaminants. Post-weld heat treatment is not normally required or suggested for HR-235[®] alloy. Heat treatment of welded fabrications may be required for other reasons, such as stress relief.

Tempe	erature	వి వి వి వి	2% trength	Y 3' 3' 2'A.T	Tensile ngth	Elongation
°F	°C	ksi	MPa	ksi	MPa	%
RT	RT	88.1	607	105.3	726	30
200	93	43.6	300	94.0	648	43
400	204	43.1	297	99.5	686	42
600	316	38.8	268	82.6	570	26
800	427	35.3	243	76.5	527	27
1000	538	37.6	259	86.1	594	38
1200	649	32.8	226	65.1	449	25
1400 🧹	760	28.2	194	54.3	374	22
1600 🧹	871 🗸	22.1	152	29.6	204	31
/ 1800 /	982 🗸	11.0	76	15.9	/ / 110 /	34 /
2000	1093	5.3	37	7.7	53	37

Tensile Properties of Welded Material Transverse Tensile – GTAW Welded Sheet

Transverse Tensile – GTAW Welded Plate

Tempe	erature		2% trength	Ultimate Stre	e Tensile ngth	Elongation
°F / /	°C	ksi	MPa	🧹 ksi 🖉 🖉	MPa	%
RT	RT	65.3	450	112.3	774	51/ /
200	93	56.2	387 🖉	89.8	619	/ / 19/ /
400	204	48.2	332	96.4	665	41/
600	316	45.6	314	90.0	621	40
800	427	42.3	292	89.1	614	44
1000	538	44.1	304	74.2	512	23
1200	649	38.1	263	73.5	507	30
1400	760	37.1	256	60.8	419	13
1600	871	23.9	165	33.1	228	25
1800	982	12.3	85	17.9	123	17
2000	1093	7.2	50	9.8	68	19

Welding Continued

Tempe	erature	S S S	Yield ngth	S S S	e Tensile ngth	Elongation	Reduction of Area
°F	°C	ksi	MPa	ksi	MPa	%	%
RT	RT	80.0	552	115.3	795	26	30
200	93	69.2	477	101.2	698	31	32
400	204	66.7	460	98.3	678	27	27
600	316	67.0	462	94.4	651	26	35
800	427	63.0	434	89.9	620	30	30
1000	538	58.9	406	82.5	569	29	37
1200	649	52.0	359	71.6	494	22	31
1400	760	48.3	333	64.8	447	16	24
1600	871	26.3	/ 181 /	36.3	250	21	23
1800	982	15.3	/ 105 /	20.7	143	15	/ /10/ /
2000	1093	9.1	63 🧹	12.0	83	20	/ 15/

AWM (All Weld Metal) Tensile – GTAW

Specifications and Codes

Specifications

HAYNES [®] HR-23 (N06235	
Sheet, Plate & Strip	ASTM B168
Billet, Rod & Bar	ASTM B166
Coated Electrodes	
Bare Welding Rods & Wire	
Seamless Pipe & Tube	ASTM B167
Welded Pipe & Tube	ASTM B619 ASTM B626
Fittings	
Forgings	
DIN	
ΤÜV	
Others	

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